

# From controllability to motion planning for mechanical systems

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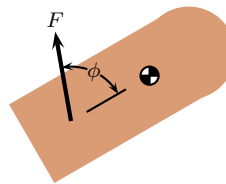
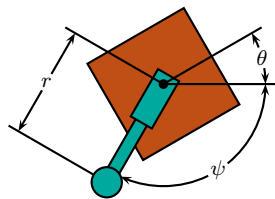
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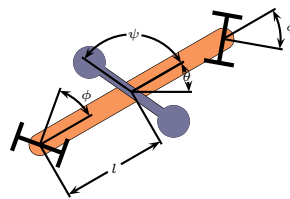
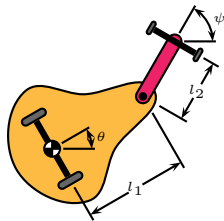


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## Some sample systems



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## What are we interested in?

- Broadly, a general methodology that encompasses modelling, analysis, and design.
- More specifically, for one of the example systems, or any system “like” them,

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- can we model it in a unified manner that is conducive to the further objectives of analysis and design?
- can one describe its reachable set?
- if given a suitable cost function, can one analyse the corresponding extremals of the optimal control problem?
- are there simple collections of trajectories that are sufficiently rich to do motion planning?

## Modelling

- For us, a **simple mechanical control system** consists of a 6-tuple  $(Q, \mathbb{G}, V, F, \mathcal{D}, \mathcal{F} = \{F^1, \dots, F^m\})$  where
  1.  $Q$  is a finite-dimensional configuration manifold,
  2.  $\mathbb{G}$  is a Riemannian metric on  $Q$ ,
  3.  $V$  is a potential function on  $Q$ ,
  4.  $F$  represents all non-potential forces that are not controlled (e.g., dissipative forces),
  5.  $\mathcal{D}$  is a distribution on  $Q$  modelling linear velocity constraints,
  6.  $\mathcal{F}$  is a collection of one-forms on  $Q$ , each representing a force over which we have control.
- The equations of motion are the Euler-Lagrange equations with Lagrangian  $L(v_q) = \frac{1}{2}\mathbb{G}(v_q, v_q) - V(q)$ , with external force  $F + \sum_{a=1}^m u_a F^a$ , and subject to the nonholonomic constraints specified by  $\mathcal{D}$ .

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- We generally simplify to the situation where  $V = 0$  and  $F = 0$ , although potential forces have received some attention,<sup>1</sup> as have dissipative forces.<sup>2</sup>

- With these simplifications, the problem is reduced to an **affine connection control system** which is described by a 4-tuple

$$\Sigma_{\text{aff}} = (\mathbb{Q}, \nabla, \mathcal{D}, \mathcal{Y} = \{Y_1, \dots, Y_m\}) \text{ with}$$

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1.  $\mathbb{Q}$  as before,
2.  $\nabla$  an affine connection (which is not generally Levi-Civita),
3.  $\mathcal{D}$  a distribution to which  $\nabla$  restricts,
4.  $\mathcal{Y}$  a collection of vector fields on  $\mathbb{Q}$  (these are related to the one-forms  $\mathcal{F}$ ).

<sup>1</sup>L/Murray, *SIAM J. Control Optim.*, **35**(3), 766–790, 1997.

<sup>2</sup>Cortés/Martínez/Bullo, *IEEE Trans. Automat. Control*, submitted, July 2001.

- When  $\mathcal{D} = T\mathbb{Q}$  then  $\nabla$  is the Levi-Civita affine connection  $\overset{\mathbb{G}}{\nabla}$  associated with  $\mathbb{G}$ .
- When  $\mathcal{D} \subsetneq T\mathbb{Q}$  then  $\nabla$  is defined by

$$\nabla_X Y = \overset{\mathbb{G}}{\nabla}_X Y - (\overset{\mathbb{G}}{\nabla}_X P)(Y),$$

where  $P$  is the orthogonal projection onto  $\mathcal{D}^\perp$ .

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- The equations of motion for such systems are

$$\nabla_{\dot{\gamma}(t)} \dot{\gamma}(t) = \sum_{a=1}^m u_a(t) Y_a(\gamma(t))$$

for a controlled trajectory  $(\gamma, u)$  satisfying  $\dot{\gamma}(t) \in \mathcal{D}_{\gamma(t)}$  for some (and hence all)  $t$ .

## Controllability

- Questions: Starting from rest at  $q_0 \in Q$  does the set of reachable configurations

1. have a nonempty interior? (accessibility)
2. contain  $q_0$  in its interior? (controllability)

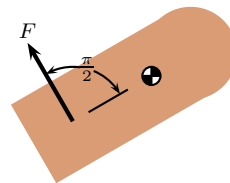
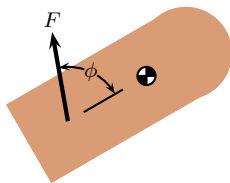
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- Accessibility is “easy” and beautiful (combine Sussmann/Jurdjevic with affine differential geometry)<sup>1</sup>.
- Controllability is quite difficult. Preliminary (and quite unsatisfactory) results were found by L/Murray.<sup>2</sup>
- It is possible to show that any (analytic) single-input system will be controllable only on a strict analytic subset.

<sup>1</sup>L/Murray, *SIAM Review*, **41**(3), 555–574, 1999

<sup>2</sup>Ibid.

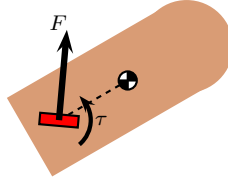
- Let's consider an example:



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|--|---|
| <ul style="list-style-type: none"><li>○ accessible</li><li>○ controllable (“easy”)</li></ul> | <ul style="list-style-type: none"><li>○ accessible</li><li>○ not controllable (not so “easy”)</li></ul> |
|--|---|

- Add more stuff to the model:



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- Controllability now goes from “not so easy” to “requiring new techniques.”<sup>1,2</sup>
- The new techniques involve the vector-valued quadratic form

$$B_y(q_0): \mathcal{Y}_{q_0} \times \mathcal{Y}_{q_0} \rightarrow T_{q_0}Q/\mathcal{Y}_{q_0}$$

$$(v_1, v_2) \mapsto \pi_{\mathcal{Y}_q}(\langle V_1 : V_2 \rangle(q_0)),$$

where

$$\langle V_1 : V_2 \rangle = \nabla_{V_1} V_2 + \nabla_{V_2} V_1$$

is the **symmetric product**.

<sup>1</sup>Hirschorn/L, *Proceedings of 40th IEEE CDC*, 4216–4221, Dec. 2001.

<sup>2</sup>Bullo/L, submitted to *SIAM J. Control Optim.*, January 2003.

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- Using the vector-valued quadratic form ideas one can prove a general result for two-input affine connection control systems which says, roughly, that they are either controllable in a very nice way, or they are controllable only on an analytic set.<sup>1</sup>
- The hovercraft with the fan dynamics is of the “only controllable on an analytic set” sort.
- Is there some sort of measure of “robustness” of controllability?

<sup>1</sup>Tyner/L, submitted to CDC03.

## Motion planning

- Question: If a system is controllable, is it possible to steer from rest at  $q_1 \in Q$  to rest at  $q_2 \in Q$ ?
- The approach is to find a collection of “motion primitives” that are rich enough to allow one to solve the motion planning problem by concatenation of primitives.

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- What sort of primitives should one look for?
- We consider **decoupling vector fields**. These are vector fields on  $Q$  whose integral curves, and any reparameterisation of them, can be followed by trajectories of the mechanical system.
- The idea is that given a rich enough class of decoupling vector fields, one solves the motion planning problem by concatenating their integral curves.

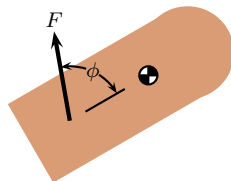
- There is a nontrivial connection between the vector-valued quadratic form used in controllability and the notion of a decoupling vector field:

**Theorem**<sup>1</sup>  $X$  is a decoupling vector field if and only if  $X$  is  $\mathcal{Y}$ -valued and  $B_{\mathcal{Y}}(X, X) = 0$ .

**“Theorem”** If  $\dim(\mathcal{Y}) = \dim(Q) - 1$  then the existence of enough decoupling vector fields for motion planning can be decided using  $B_{\mathcal{Y}}$ .

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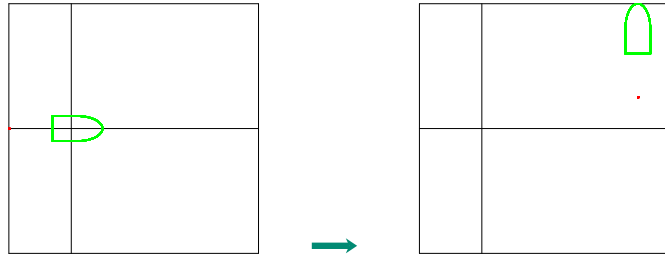
- What about our example?



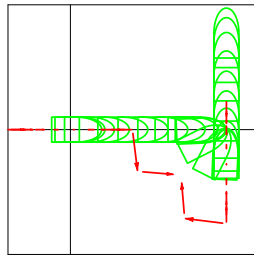
- Controllable, as we have seen.
- Possible to find enough decoupling vector fields.
- There are two. What are they?

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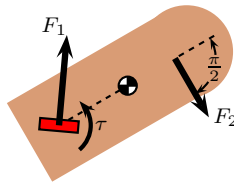
<sup>1</sup>Bullo/Lynch, *IEEE Trans. Robotics and Autom.*, **17**(4), 402–412, 2001.



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- What about the more complicated model?
- It is not controllable, so it needs one more input:

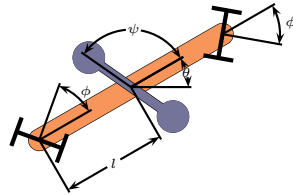


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- The theory predicts there are enough decoupling vector fields to do motion planning.
- Last week Dave Tyner found them.
- Are they simple enough to do anything with?

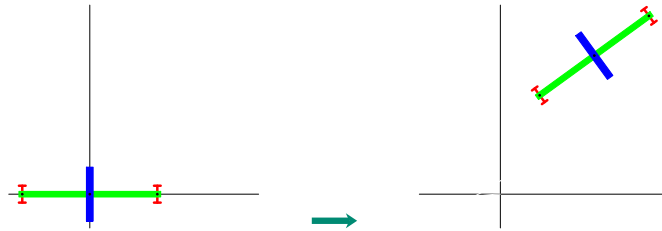
## A not so easy example

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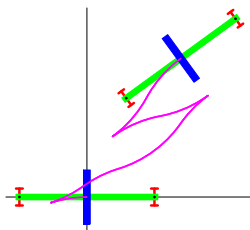


- accessible.
- controllable.

- The system also possess enough decoupling vector fields to do motion planning.
- This can be done explicitly!



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## What else?

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- We have an actual hovercraft, and the open-loop motion planning primitives work *extremely* poorly.
- Linearise around trajectories to stabilise them in closed-loop.
- Understand non-ideal model effects (friction, actuator magnitude and rate constraints, etc.)